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EASEE-gas

European Association for the Streamlining of Energy Exchange - gas

Common Business Practice

Number: 2022-001/01
Subject: Hydrogen Quality Specification
Approved: Board virtual meeting on 14 September 2021

Summary
This CBP defines the hydrogen quality specification for dedicated hydrogen pipelines.

31 **About EASEE-gas**32 <https://easee-gas.eu/about-easee-gas>

33

34 **Version List**

35

Number/ Version	Approved	Implementation date
(2022-001)/01		Already in place

36

37 **Reference List**

38

Reference	Document name	Version
	EASEE-gas Reference CBP Hydrogen Quality Specification	V 1.0*

39

40 **Common Business Practice 2022-001/01 “Hydrogen Quality**
41 **Specification”**

42
43 **1.1 APPLICATION AREA**
44

45 This CBP defines the recommended quality specification for hydrogen (non-
46 blended with natural gas, see Note 1) flowing through dedicated systems,
47 meaning networks that were originally designed and used for natural gas
48 transmission and after a safety and reliability assessment (see Note 2) found
49 suited for conveying hydrogen and newly built hydrogen pipeline systems. The
50 CBP is valid for both the entry as well as the exit points of these dedicated
51 systems.

52
53 *Note 1: This CBP is not applicable to blends of hydrogen and natural gas.*

54
55 *Note 2: This CBP only specifies the recommended hydrogen specification. Before*
56 *hydrogen can be transmitted through existing European natural gas grids, safety*
57 *and reliability assessments need to be carried out to prove the suitability of the*
58 *given grid for the transmission of hydrogen.*

59
60 *Note 3: After the pipeline is switched over from natural gas to hydrogen there is*
61 *a period in which the hydrogen composition can be influenced by natural gas*
62 *residues still present in the pipeline system. This period is referred to by the*
63 *term ‘transition period’.*

64
65 This CBP focusses on ‘industrial grade’ hydrogen because it is expected that in
66 the coming years, the large-scale production of hydrogen, necessary to operate a
67 pipeline system, will partly take place by chemical conversion of hydrocarbons.
68 In contrast to electrolysis, these processes do not deliver inherent fuel cell
69 quality hydrogen. Possibilities for large scale production of hydrogen via
70 electrolysis are not expected before 2030. Another reason to focus on ‘industrial
71 grade’ hydrogen is the observation from market forecasts that the industry will
72 take the lion part of the total hydrogen production. Only in the period after 2030,
73 there is a possibility for large scale demand for fuel cell and/or energy production
74 grade hydrogen. Last but not least, no hands-on experience is available on the
75 possible effects of residues in the pipeline resulting from the previous exposure
76 to natural gas on the hydrogen transmitted through such a pipeline. The risk that
77 small amounts of a particular contaminant result in an off-specification at the exit
78 increases with an increase of the minimum hydrogen purity.

79
80 Depending on the developments in the hydrogen production and advances in the
81 market, i.e. large market for fuel cells, it is recommended to evaluate the current
82 specification after a period of 3 years or earlier if necessary. An additional
83 advantage after the specification being in place for a number of years is that
84 more information will be available on the effect of the residues in the pipeline on
85 the hydrogen quality during the transition phase.

86 1.2 HYDROGEN QUALITY SPECIFICATION

87

88 The basis for the parameters and their limit values in this CBP is based on an
 89 internal analysis carried out by EASEE-gas in which the end user requirements,
 90 the market shares, the hydrogen quality obtained by the various production
 91 techniques and the contribution of the pipeline were taken into account and a
 92 common denominator was defined.

93

94 *Note 4: It is acknowledged that this specification will not meet the specific*
 95 *requirements of some of the industrial (feedstock) users and therefore needs on-*
 96 *site pre-treatment. Especially the strict requirements regarding sulphur*
 97 *components requires in most cases on-site desulphurisation. Furthermore, it is*
 98 *noted that the oxygen limitations in some of the industrial processes are more*
 99 *strict i.e. a maximum 24 hour moving average value of 5 ppm (molar basis)*
 100 *oxygen (O₂) and a maximum hourly value of 25 ppm (molar basis) oxygen (O₂).*

101

102 The parameters and limit values that have been agreed upon for this CBP and
 103 are given in the table below. A short explanation for some of the parameters and
 104 their limit values can be found in the explanatory notes section.

105

Parameter	Unit	Min	Max
Hydrogen	mol-%	98,0	-
Carbon monoxide	ppm	-	20
Total sulphur content ¹	mg S/m ³ (n) ²	-	21 ⁽³⁾
Carbon dioxide	ppm	-	20
Hydrocarbons (including Methane)	mol-%	-	1,5 ⁽³⁾
Inerts (Nitrogen, Argon, Helium)	mol-%	-	2,0
Oxygen	ppm (mol)	-	10 ^(4,5)
Total halogenated compounds	ppm (mol)	-	0,05
Water dewpoint	°C at 70 bar(a)	-	- 8
Hydrocarbon dewpoint ³	°C at 1-70 bar(a)	-	- 2 ⁽³⁾

1) Non-odorised hydrogen

2) normal conditions (1.01325 bar(a), 0 °C)

3) During the transition period, where the hydrogen composition can be influenced by natural gas residues present in the pipeline system (see Note 5)

4) Expressed as expressed as a moving 24-hour average

5) Where the hydrogen can be demonstrated not to flow to installations or end-user applications sensitive to higher levels of oxygen, (e.g. feed stock users or hydrogen storages), a higher limit of up to 1000 ppm may be applied.

106

107 *Note 5: It is acknowledged that the presence of residues in the pipeline as a*
108 *result of natural gas transmission, makes it necessary to relax the specification*
109 *for the total sulphur content, to allow for higher hydrocarbons to be present and*
110 *to introduce a temporary specification for the hydrocarbon dewpoint.*

111

112 The gas shall not contain constituents other than listed in the table above at
113 levels that prevent its transportation, storage and/or utilization without quality
114 adjustment or treatment.

115

116 **1.3 EXPLANATORY NOTES**

117

118 **1.3.1 EXISTING SPECIFICATIONS**

119

120 Although a number of specifications for various grades of 'pure' hydrogen exist,
121 none of these specifications for 'pure' hydrogen are suitable as a general
122 specification for hydrogen flowing through a former natural gas network without
123 modifications.

124

125 The specification for a hydrogen grade used for Proton exchange membranes
126 refers to hydrogen with a very high purity (minimum 99,97 mol-% H₂). This very
127 high purity hydrogen can neither be guaranteed in a 'former' natural gas network
128 nor is it necessary for the larger part of the hydrogen end consumers. On the
129 other hand, the lower grade hydrogen specifications don't contain the necessary
130 limit values for parameters normally encountered in natural gas like for example
131 the water dewpoint and are therefore not suitable.

132

133 **1.3.2 HYDROGEN CONTENT**

134

135 Based on the inventory carried out by EASEE-gas a hydrogen concentration equal
136 or higher than 98 mol-% is proposed. This is in agreement with the hydrogen
137 purity stated for Grade A in ISO 14687:2019 standard.

138

139 **1.3.3 CHOICE OF TRACE COMPONENTS IN THE SPECIFICATION**

140

141 Depending on the hydrogen production technique used and the condition of the
142 network, a large number of trace components can in principle be present in the
143 hydrogen. EASEE-gas has chosen to only specify critical components.

144

145 **1.3.4 CARBON MONOXIDE**

146

147 If the production of hydrogen gas takes place by reforming, carbon monoxide is
148 one of the constituents present. The requirements regarding the carbon
149 monoxide content for the various industrial processes and appliances show a
150 wide range of values but most of them are in the ppm range. A value of 20 ppm
151 is a compromise between the hydrogen production and the usability by the
152 various end user categories. In the Hy4Heat study (1), which was the basis for
153 the BSI PAS 4444 standard, a similar conclusion was drawn.

154 **1.3.5 SULPHUR COMPONENTS**

155

156 A source of sulphur components, like hydrogen sulphide and mercaptans, is the
157 (natural) gas used in a reforming process. Since sulphur components are
158 poisoning the catalysts used in the various types of reforming processes, the
159 sulphur components will be removed from the (natural) gas before the actual
160 reforming process takes place and thus the resulting hydrogen is almost free of
161 sulphur components.

162

163 Another source of sulphur components could be the residue left in the pipeline.
164 During the transition period, which ends for sulphur at the moment no sulphur
165 components are released anymore from the pipeline debris, the total sulphur
166 shall not be more than 21 mg S/m³ (n). This value corresponds to the
167 specification mentioned in European EN 16726 standard for H-gas.

168

169 After the transition period, the maximum amount of total sulphur is expected to
170 be much lower since most of the existing hydrogen production processes are
171 known to produce virtual no sulphur components. However, since no accurate
172 data is available at the moment no maximum value for the total sulphur content
173 after the transition phase is specified.

174

175 **1.3.6 CARBON DIOXIDE**

176

177 If the production of hydrogen gas takes place by reforming, carbon dioxide is
178 also one of the constituents present. Like for carbon monoxide, the requirements
179 regarding the carbon dioxide content for the various industrial processes and
180 appliances show a wide range of values but most of them are in the ppm range.
181 The value of 20 ppm is for carbon dioxide also a good compromise between the
182 hydrogen production costs and the usability of the hydrogen by the end users.

183

184 **1.3.7 HYDROCARBONS INCLUDING METHANE**

185

186 Methane will be mostly present in the hydrogen gas if a chemical conversion
187 process is used for its production. In most of the industrial feedstock
188 applications, methane does not take part in the chemical reaction and is
189 considered as an inert. However, the presence of a higher concentration of
190 methane in the hydrogen feedstock can result for processes in which part of the
191 feed stream is recycled to larger recycle- and vent streams and thus to higher
192 costs. On the other hand a higher hydrocarbon (methane) specification facilitates
193 the use of methanation as a purification method for hydrogen production. The
194 methanation step converts carbon monoxide and carbon dioxide into methane.

195

196 During chemical conversion most of the other hydrocarbon species present in the
197 (natural) gas will be converted into hydrogen resulting apart from methane in
198 the absence of other hydrocarbon species in the product stream.

199

200 Hydrocarbons can also originate from the residue present in the pipeline.

201

202 The amount of hydrocarbons shall not be more than 1,5 mol-%. Various end
203 users prefer to have separate specifications for the maximum allowed amount of

204 methane and the other (heavier) hydrocarbons because of the different effects
205 on their processes. Since no accurate data is available at the moment it is not
206 possible to come up with a proposal for such a split.

207

208 **1.3.8 HYDROCARBON DEWPOINT (DURING TRANSITION PERIOD)**

209

210 During the transition process of a pipeline system from (natural) gas to
211 hydrogen, it cannot be fully excluded that in the beginning hydrocarbons from
212 the pipeline residue are taken up by the hydrogen passing along. To limit the
213 maximum allowable concentration hydrocarbons, during this transition, a
214 hydrocarbon dewpoint specification is in force. The specification of ≤ -2 °C at any
215 pressures between 1 and 70 bar(a) is taken from the European standard EN
216 16726 for natural gas.

217

218 **1.3.9 INERTS**

219

220 The fraction inerts consists of argon, helium and nitrogen. The specification
221 (≤ 2 mol-%) is complementary to the hydrogen specification (≥ 98 mol-%).
222 Argon can be found as a constituent in the produced hydrogen if it is produced
223 via an Auto Thermal Reforming or Partial Oxidation reforming process.
224 Some natural gases contain nitrogen and/or helium and therefore nitrogen
225 and/or helium can be found as a constituent in the produced hydrogen gas via a
226 reforming process. Argon and helium are noble gases and do not take part in any
227 chemical reaction. Apart from the ammonia production, nitrogen does not take
228 part in the chemical reaction and is therefore also categorised as an inert.
229 Like with the hydrocarbons, large amounts of inerts can result for processes in
230 which part of the feed stream is recycled to larger recycle- and vent streams and
231 thus to higher costs. On the other hand, a higher maximum allowed
232 concentration of inerts avoids the use of Pressure Swing Adsorption as a
233 purification method for hydrogen production by reforming.

234

235 **1.3.10 OXYGEN**

236

237 For (natural) gas, according to the European standard EN 16726, a maximum
238 level of 10 ppm, expressed as a moving 24-hour average, is specified for
239 sensitive users. The production of hydrogen, both by reforming as well as
240 electrolysis can fulfil this requirement without requiring complex process steps
241 and thus high costs. Especially industrial feedstock users require an oxygen
242 content in the lower ppm range because oxygen can poison the catalysts used in
243 those chemical processes. However, where the hydrogen can be demonstrated
244 not to flow to installations or end-user applications sensitive to higher levels of
245 oxygen, , e.g. feed stock users or hydrogen storages, a higher limit of up to
246 1000 ppm may be applied.

247

248 **1.3.11 HALOGENATED COMPOUNDS**

249

250 Halogenated compounds can be present in the hydrogen gas if produced by
251 electrolysis of a sodium chloride solution or theoretically by reforming of gas
252 originating from a landfill. However, the latter is not very realistic because this
253 requires an extensive cleaning of the gas before it can be used in a reformer.

254 Furthermore, in the required purification step, which is probably based on
255 pressure swing adsorption, halogenates will preferably be trapped. This
256 specification is taken from the requirement stated in ISO 14687:2019 for Grade
257 D and Grade E.

258

259 **1.3.12 WATER**

260

261 The current specification for natural gas (EN 16726) specifies a water dewpoint
262 of -8 °C at a pressure of 70 bar(a) which matches a water content of 48 ppm (v)
263 for hydrogen. This limiting value does not fulfil the requirements for fuel cells
264 (< 5 ppm) and the production of hydrogen peroxide (< 10 ppm). However, since
265 these two applications require a higher hydrogen concentration as specified in
266 this CBP, the water dewpoint specification of -8 °C at a pressure of 70 bar(a) is
267 maintained in the CBP.

268

269 **1.3.13 WOBBE INDEX**

270

271 A Wobbe-range is not taken into account in this specification because the sum of
272 all components with the exception of hydrogen can only reach a maximum value
273 of 2 mol-%. The largest difference in Wobbe index occurs for a composition
274 existing of 98 mol-% hydrogen and 2 mol-% nitrogen and using ISO 6976 results
275 in a maximum shift of 6,1 MJ/m³ (n), or equivalently, in a maximum reduction in
276 Wobbe Index of 12,6 %.